

ISSMGE Webinar 2020

Geosynthetic-Reinforced Soil Structures – Developments from Walls to Bridges – Digest

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ISSMGE Webinar video can be seen from:

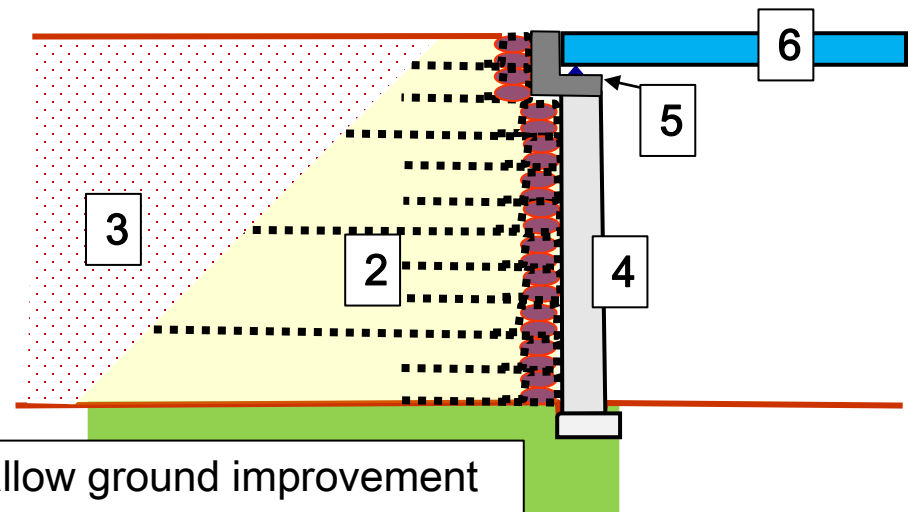
Geosynthetics-Reinforced Soil Structures -
Developments from Walls to Bridges- | ISSMGE

<https://www.issmge.org/education/recorded-webinars/geosynthetics-reinforced-soil-structures-developments-from-walls-to-bridges>

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- 1. Recent typical GRS structures for railways in Japan**
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7. Concluding remarks

GRS Bridge Abutment



1. Shallow ground improvement
when necessary

13.4 m-high, Mantaro site



Under construction
Oct. 2011



Completed
Aug. 2012

Construction sites of GRS RWs with FHR facing & the related other GRS structures (as of June 2019)

Total wall length: 184 km

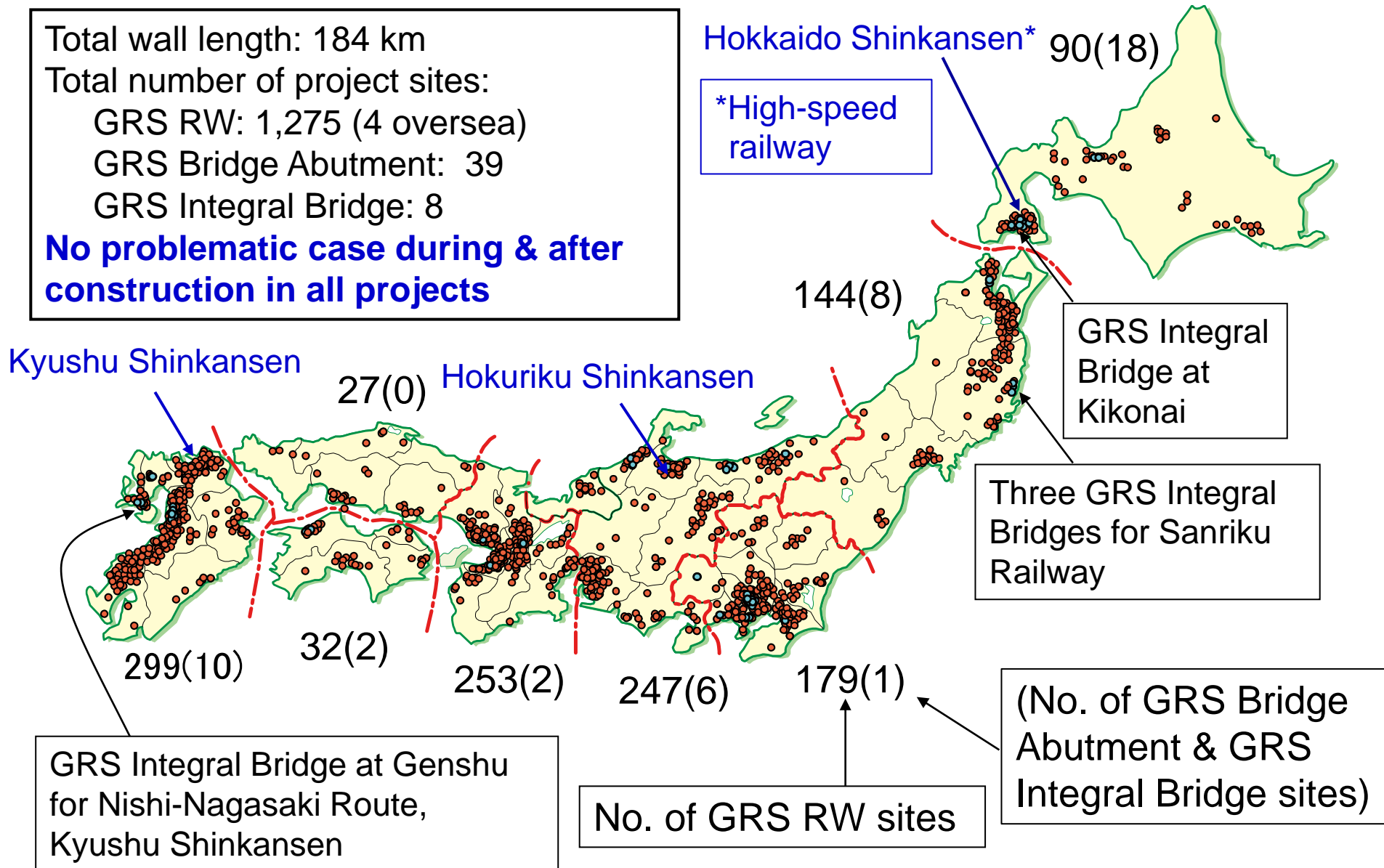
Total number of project sites:

GRS RW: 1,275 (4 overseas)



GRS Bridge Abutment: 39

GRS Integral Bridge: 8

No problematic case during & after construction in all projects



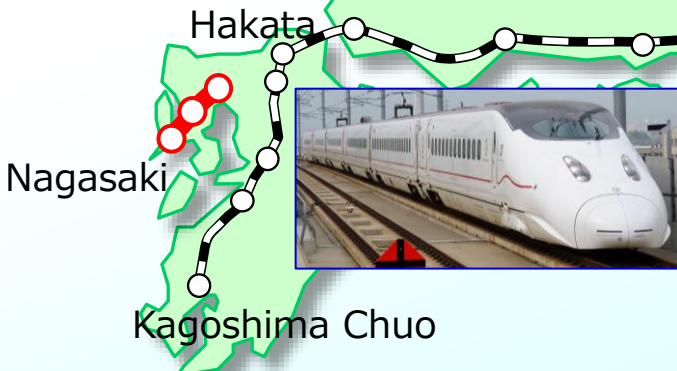
Shinkansen (High Speed Railway), January 2019

	In service	2,764.5 km (since 2000, 929.4 km)
 Under construction	Hokkaido (extension)	211.5km
	Hokuriku (extension)	125.2km
	Kyushu (Nagasaki route)	66.0km

Kyushu
(Nagasaki route)
to be completed
2022



Hokuriku



Tsuruga
Shin-Osaka
Nagoya
Omiya
Tokyo

Tokaido
opened Oct. 1964

Shin-Hakodate
Hokuto

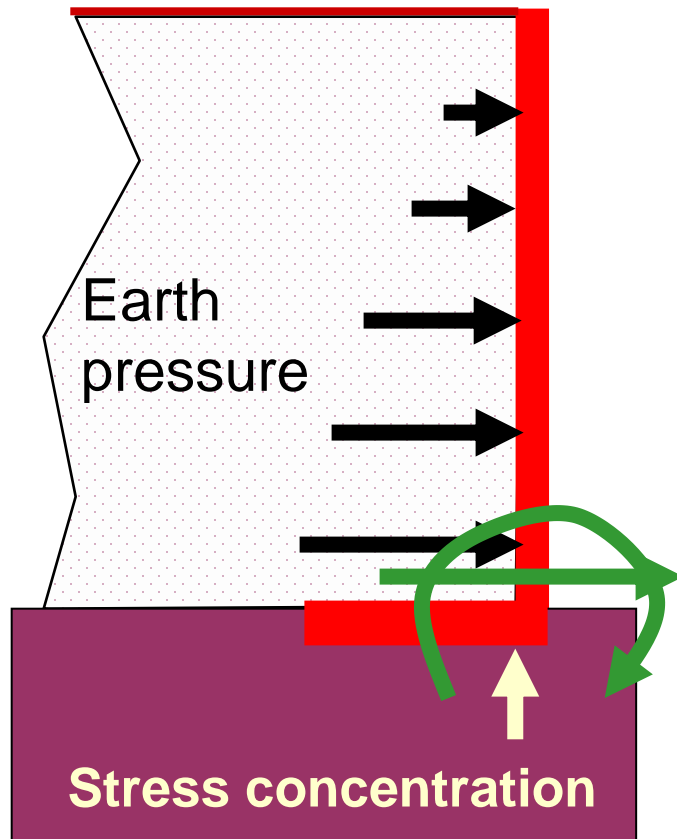
Hokkaido
opened
March 2016

Sapporo

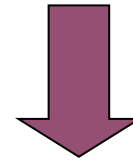
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Conventional RW is a cantilever structure



- Large forces in the facing
- Large overturning moment & large lateral load at the facing base

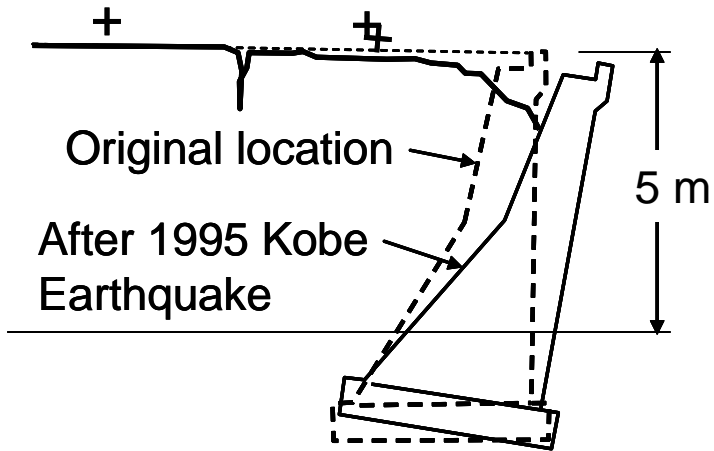


Need for a massive strong facing structure and a pile foundation

Relatively unstable, particularly against seismic loads

1995 Kobe Earthquake

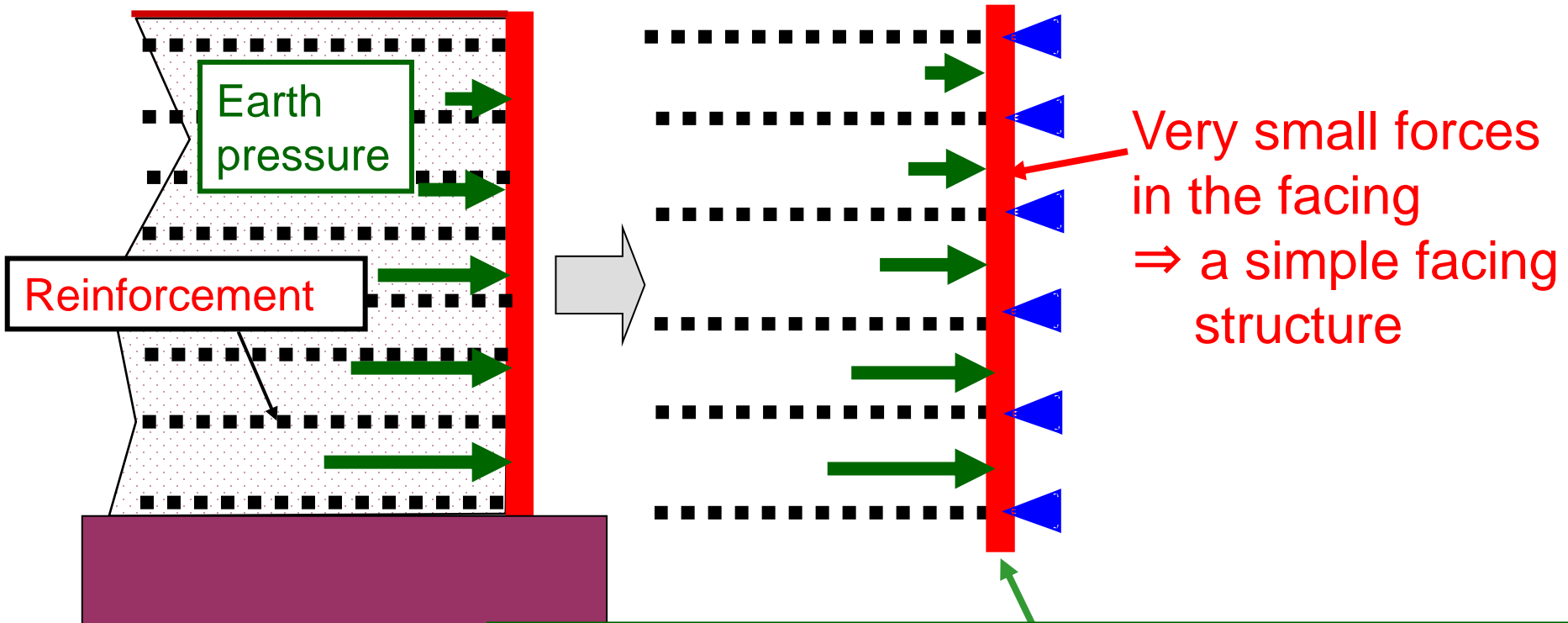
Collapse of gravity type walls at Ishiyagawa



Collapse of gravity type walls, despite seismic design using $k_h = 0.2$ with $(F_s)_{\text{allowable}} = 1.5$

GRS RW with full-height rigid (FHR) facing:

FHR facing is “a continuous beam supported by many reinforcement layers at a small span”

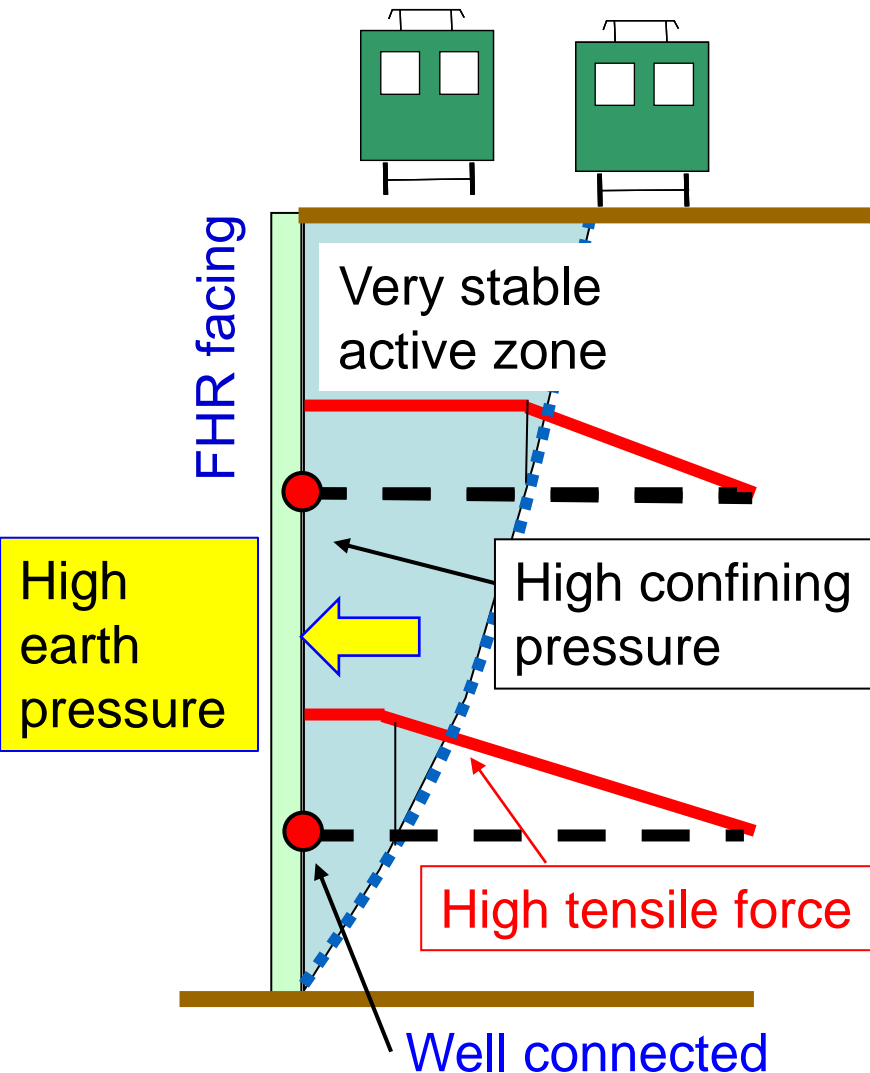


Small overturning moment & lateral force at the facing base

⇒ no need for a pile foundation

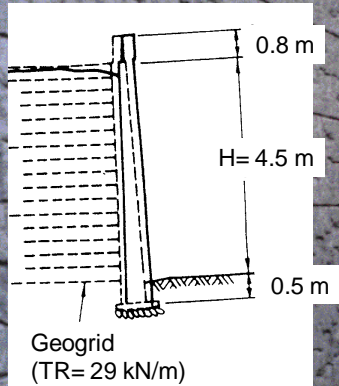
⇒ stable, particularly against seismic loads¹⁰

Importance of firm connection between FHR facing and reinforcement layers



- High earth pressure at the wall face
- High tensile forces in the reinforcement
- In the active zone, high confining pressure, therefore, high strength & stiffness of the backfill
- High stability of the wall

Immediately after completion, 1992



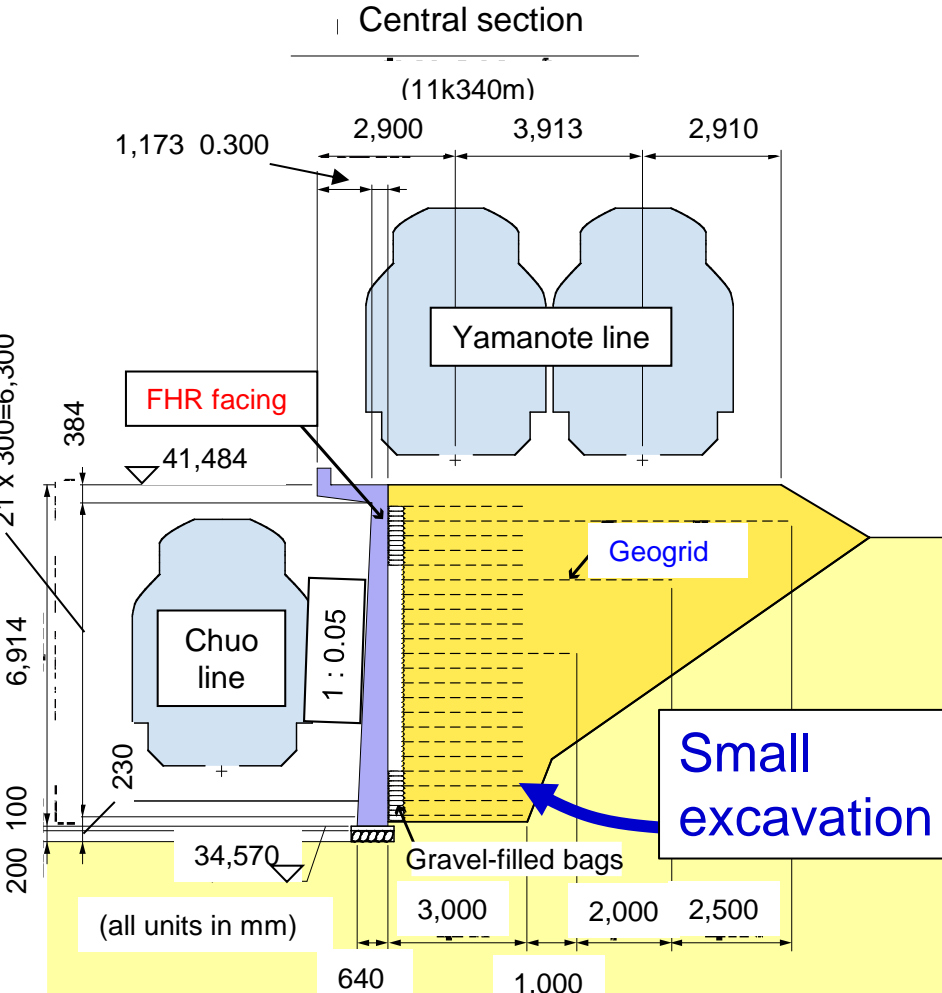
GRS RW with a FHR facing
for a rapid transit at Tanata

A week after the 1995 Kobe Earthquake



The wall survived!

GRS RW with FHR facing supporting very busy urban railway



Near Shinjuku Station, Tokyo,
constructed during 1995 – 2000

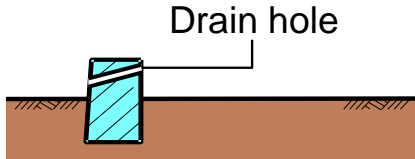


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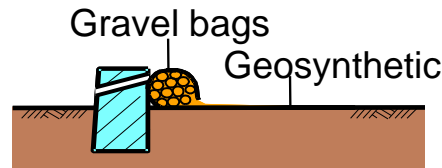
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Staged construction: 1) & 2)

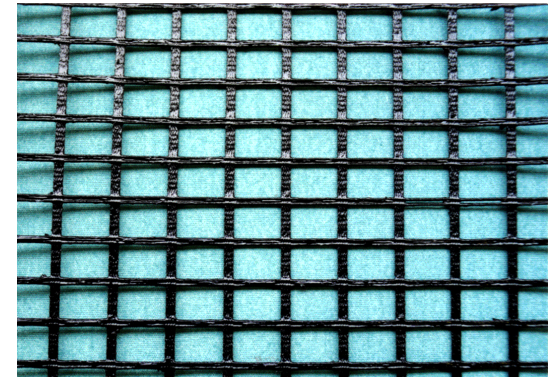
- Construction with a help of gravel bags placed at the shoulder of each soil layer



1) Levelling pad for facing



2) Placing geosynthetic & gravel bags

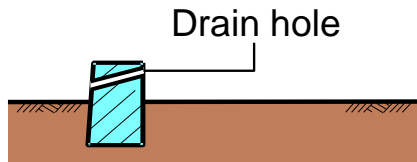


10 cm

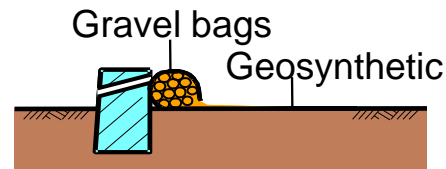
Typical polymer geogrid:
bi-axial PVA grid (very high
resistance against high PH:
& high anchorage strength)

Staged construction: 3) & 4)

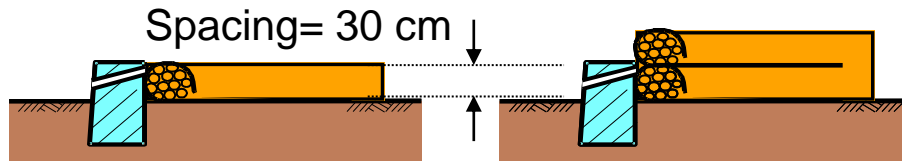
- Compaction of backfill with a help of gravel bags placed at the shoulder of each soil layer



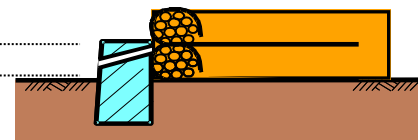
1) Levelling pad for facing



2) Placing geosynthetic & gravel bags



3) Backfilling & compaction



4) Second layer



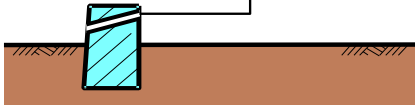
Good compaction of the backfill by:

- 1) a small lift (15 cm) resulting from a small vertical spacing (30 cm) of geogrid layers; and
- 2) no rigid facing during backfill compaction

Staged construction: 5)

- Completing the full-height wall without FHR facing

Drain hole



1) Levelling pad for facing

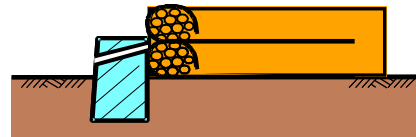
Gravel bags
Geosynthetic



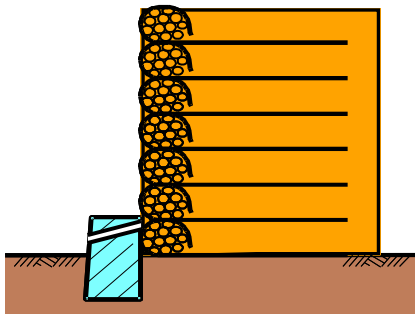
2) Placing geosynthetic & gravel bags



3) Backfilling & compaction



4) Second layer

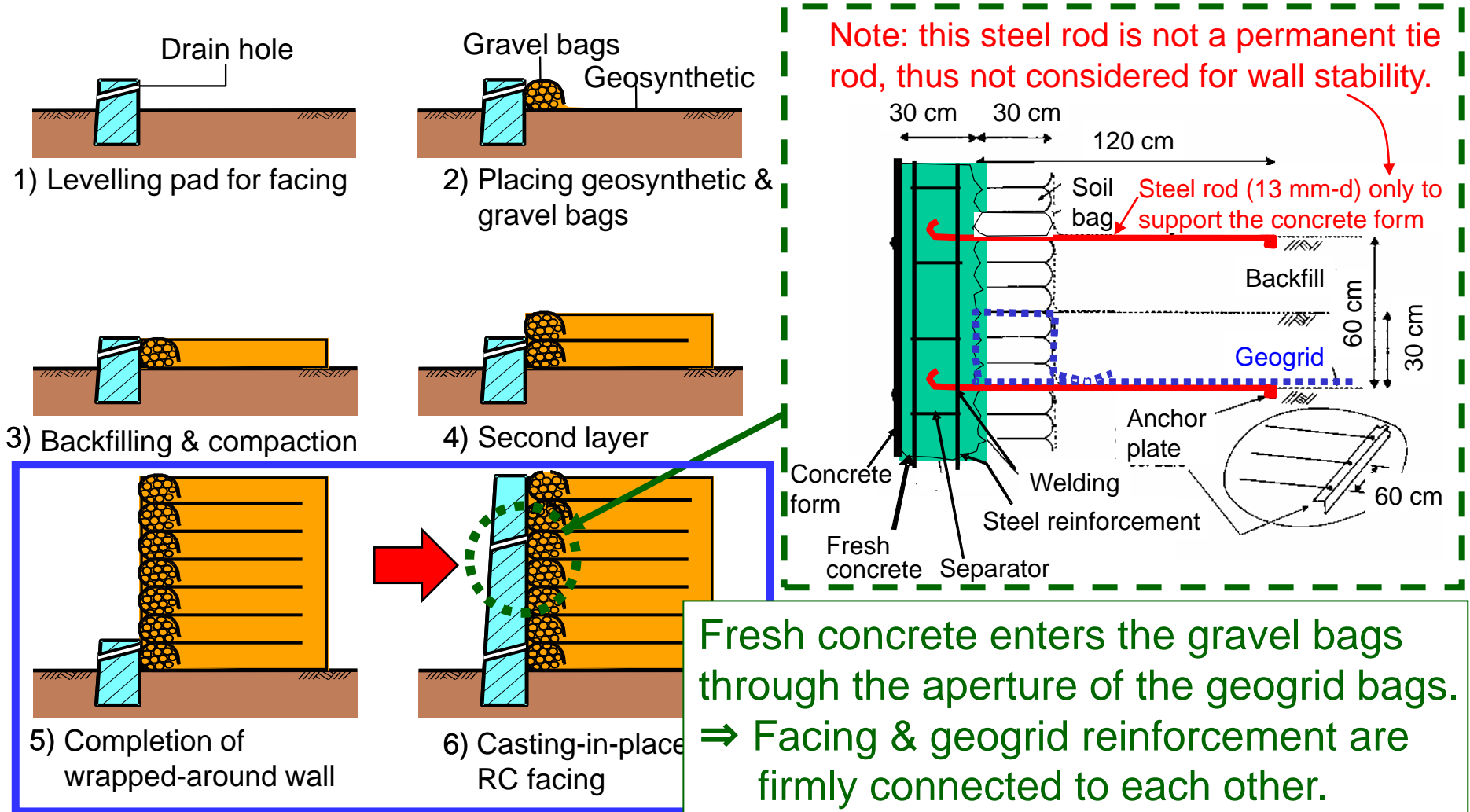


5) Completion of wrapped-around wall



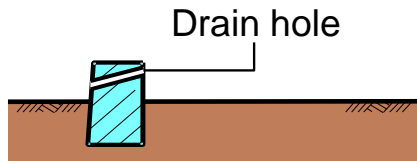
Staged construction: from 5) to 6)

- After sufficient compression of backfill and subsoil has taken place, a full-height rigid (FHR) facing is constructed by casting-in-place fresh concrete directly on the wrapped-around wall.

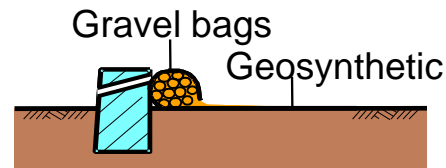


Staged construction: from 5) to 6)

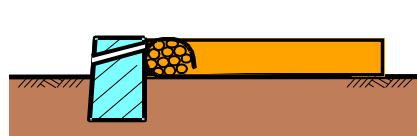
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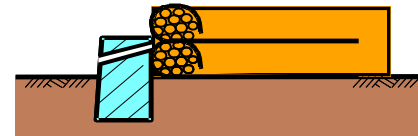
1) Levelling pad for facing



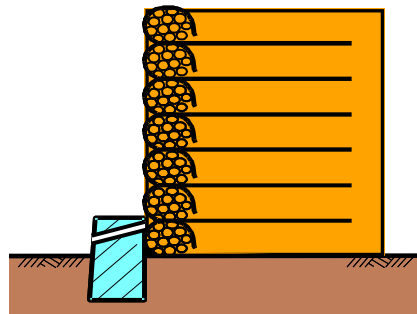
2) Placing geosynthetic & gravel bags



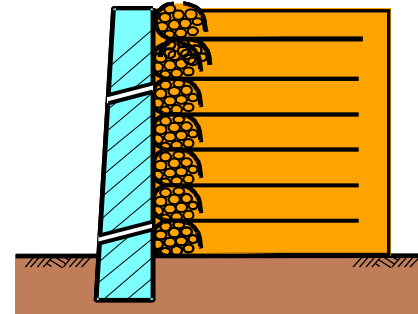
3) Backfilling & compaction



4) Second layer



5) Completion of wrapped-around wall



6) Casting-in-place RC facing

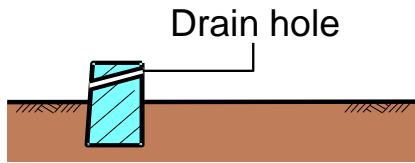
→ After step 6), the differential settlement between the FHR facing and the backfill becomes very small.

→ The facing/geogrid connection is not damaged during service of completed wall.

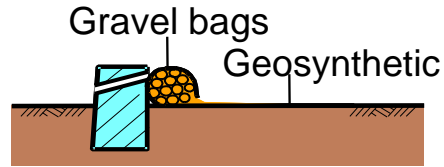
→ Construction using compressive backfill and/or on a compressive subsoil becomes possible.

Staged construction – 6)

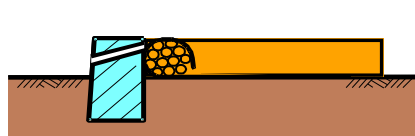
Competition



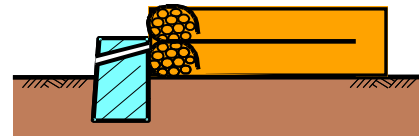
1) Levelling pad for facing



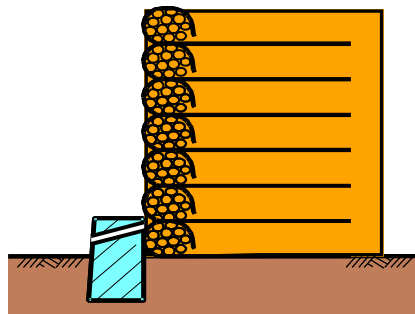
2) Placing geosynthetic & gravel bags



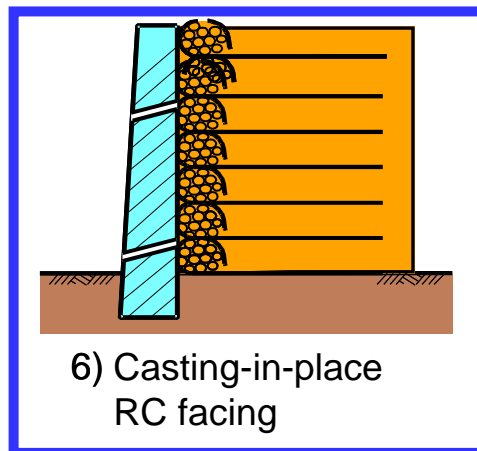
3) Backfilling & compaction



4) Second layer



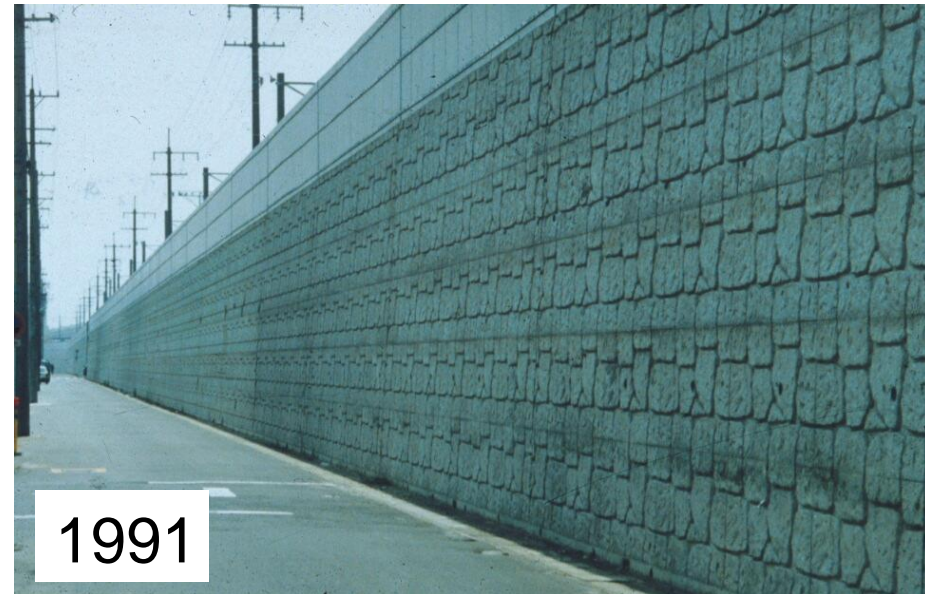
5) Completion of wrapped-around wall



6) Casting-in-place RC facing

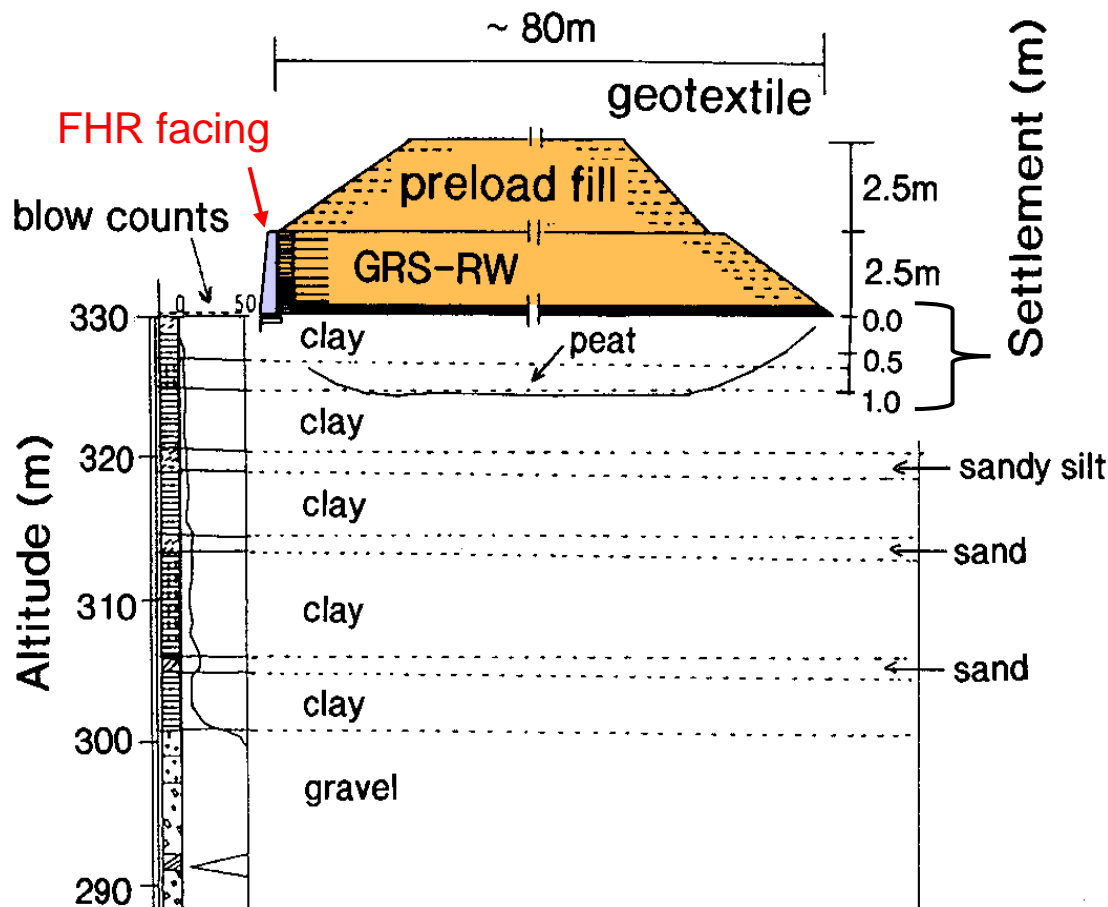
A typical case:

Re-construction of a gentle slope to a vertical wall for a yard of Shinkansen at Biwajima, Nagoya



Nagano wall:

- for a yard for Shinkansen
- 2.0 m-high & 2 km-long
- constructed 1993 - 1994



a) Backfill: **nearly saturated soft clay**

b) Constructed on a thick very soft clay deposit

- no pile foundation

- **staged construction:**

1) GRS RW w/o FHR facing

2) preload fill

3) settlement (about 1 m)

4) removal of preload fill

5) construction of FHR facing

Preloading wall height

before preloading: 3.0 m

after preloading: 2.0 m

Construction of FHR facing
after removing the preload fill.



20 years after construction,
6th July 2014

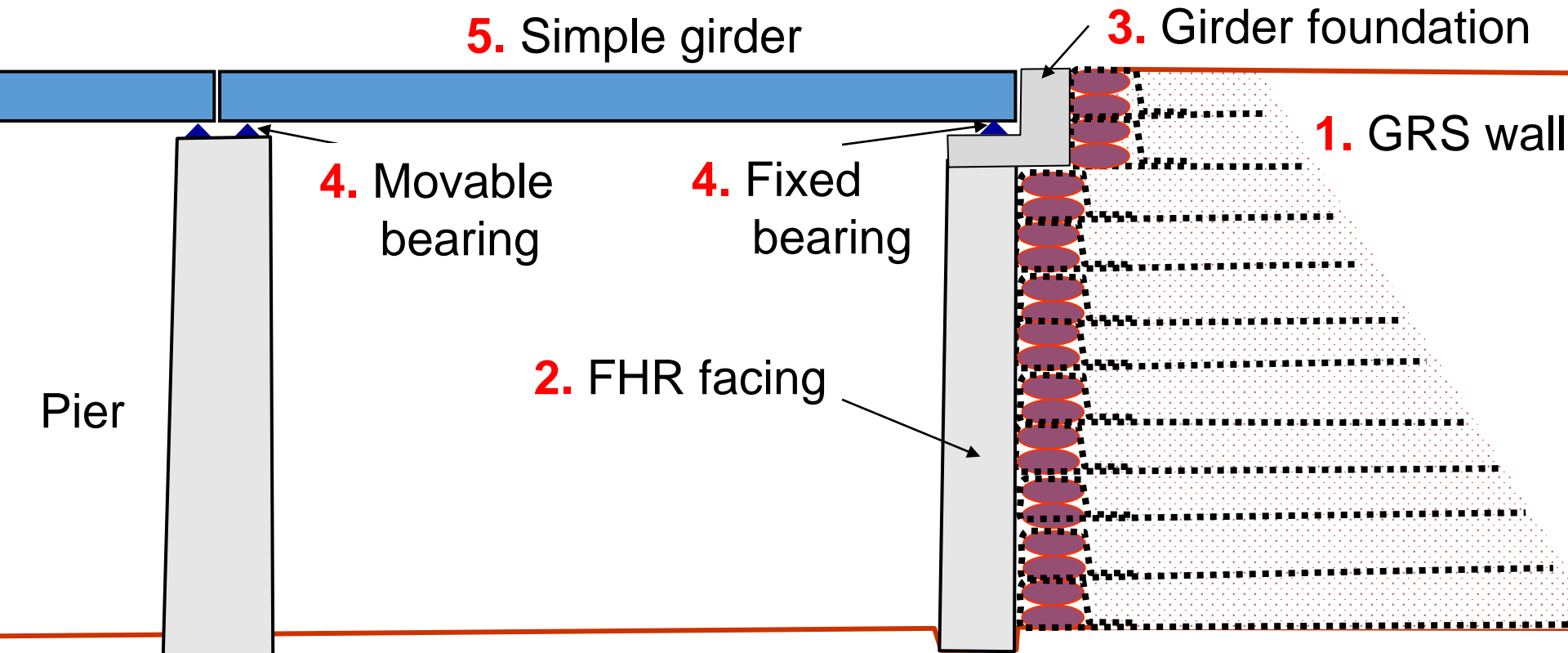


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GRS Bridge Abutment

The girder foundation becomes much more stable by structural integration to the top of the FHR facing



Much more cost-effective and much more stable than conventional type bridge abutments; and statically determinate, thus not sensitive to residual displacements of the FHR facing \Rightarrow rather simple to design

GRS Bridge Abutment

First GRS Bridge Abutment
at Takada for Kyushu Shinkansen

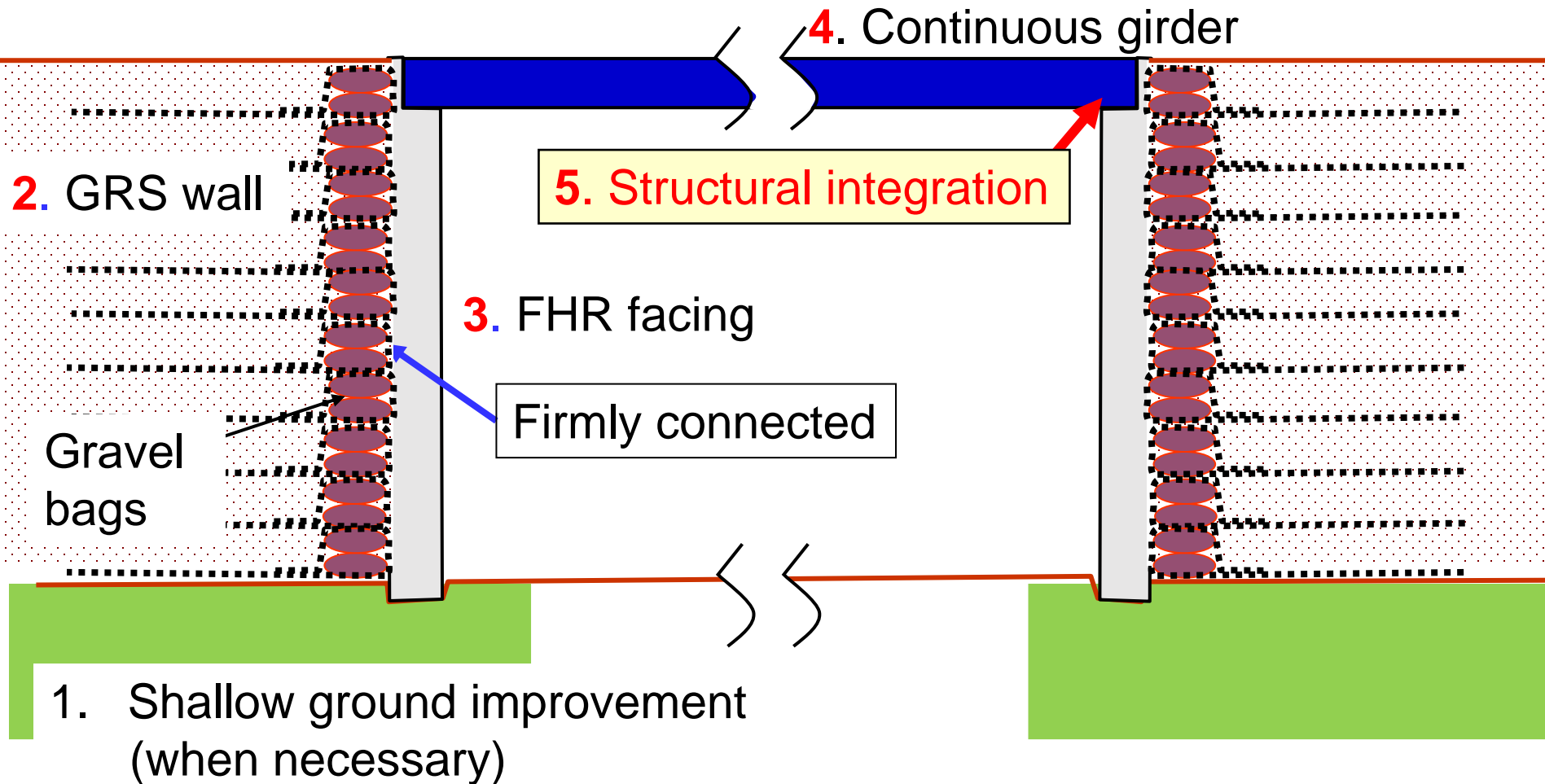


GRS Bridge Abutment at Mantaro
for Hokkaido Shinkansen



- After the construction of the first one at Takada in 2003,
- by 2018, 36 have been constructed and are in service; and
 - many others are at the design stage or under construction, including 80 for Kyushu Shinkansen Nagasaki Route.

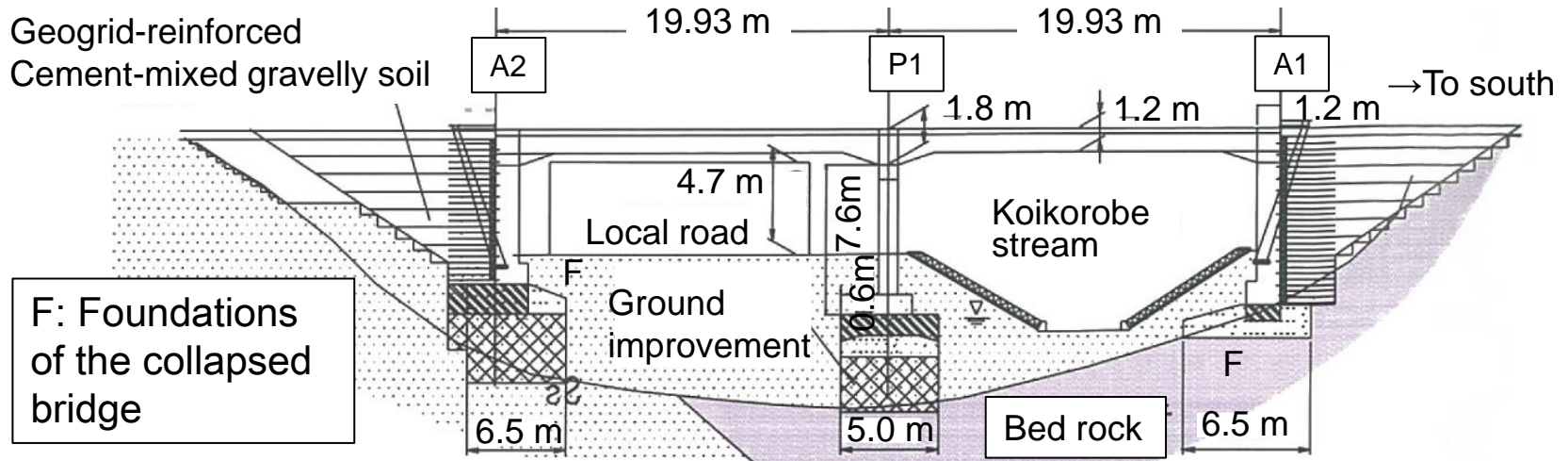
GRS Integral Bridge (not using girder bearings)



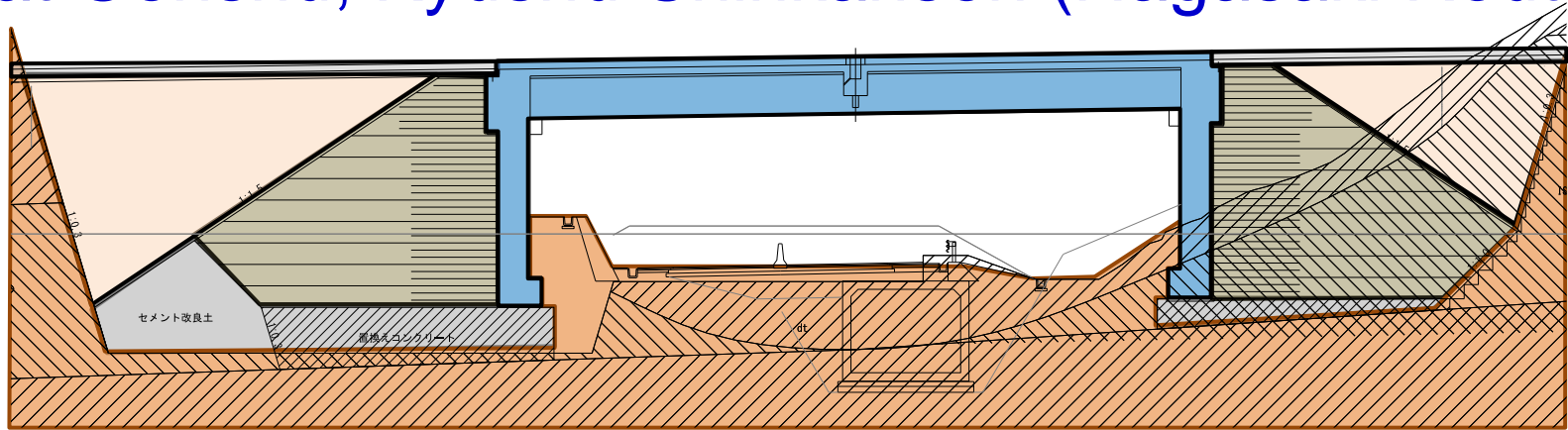
20 days after the 2011 Great East Japan E.Q.
(11 March 2011)
Koikoreobe, Sanriku Railway.



GRS Integral Bridge at Koikorobe, Sanriku Railway



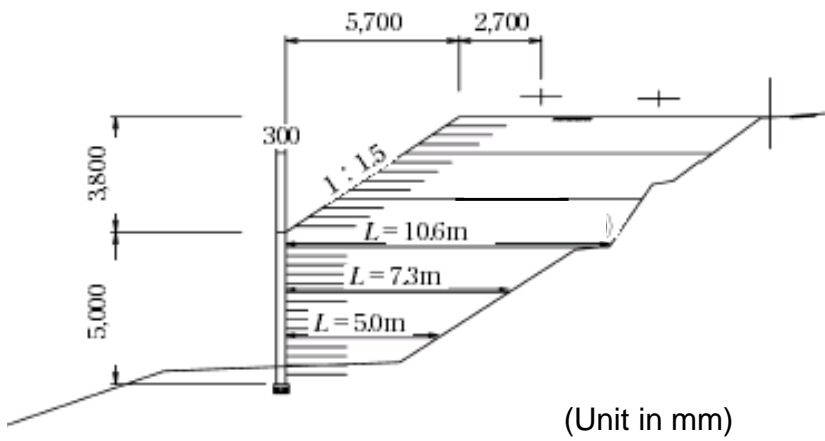
The latest GRS Integral Bridge at Genshu, Kyushu Shinkansen (Nagasaki Route)



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2004 Niigata-ken Chuetsu EQ, October 2004



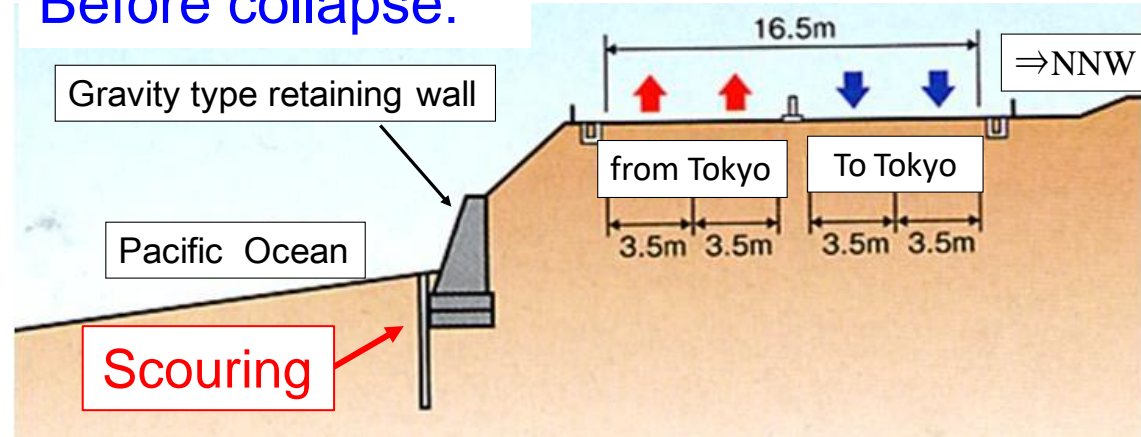
Site 3



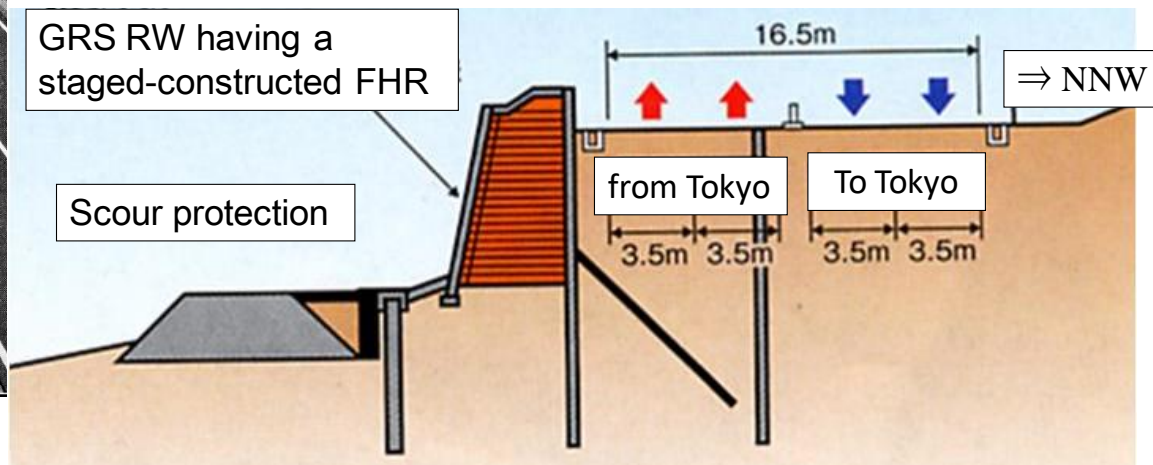
Collapse of gravity-type seawall for a length of 1.5 km by Typhoon No. 9, 8 Sept. 2007 (National Road No. 1, southwest of Tokyo)



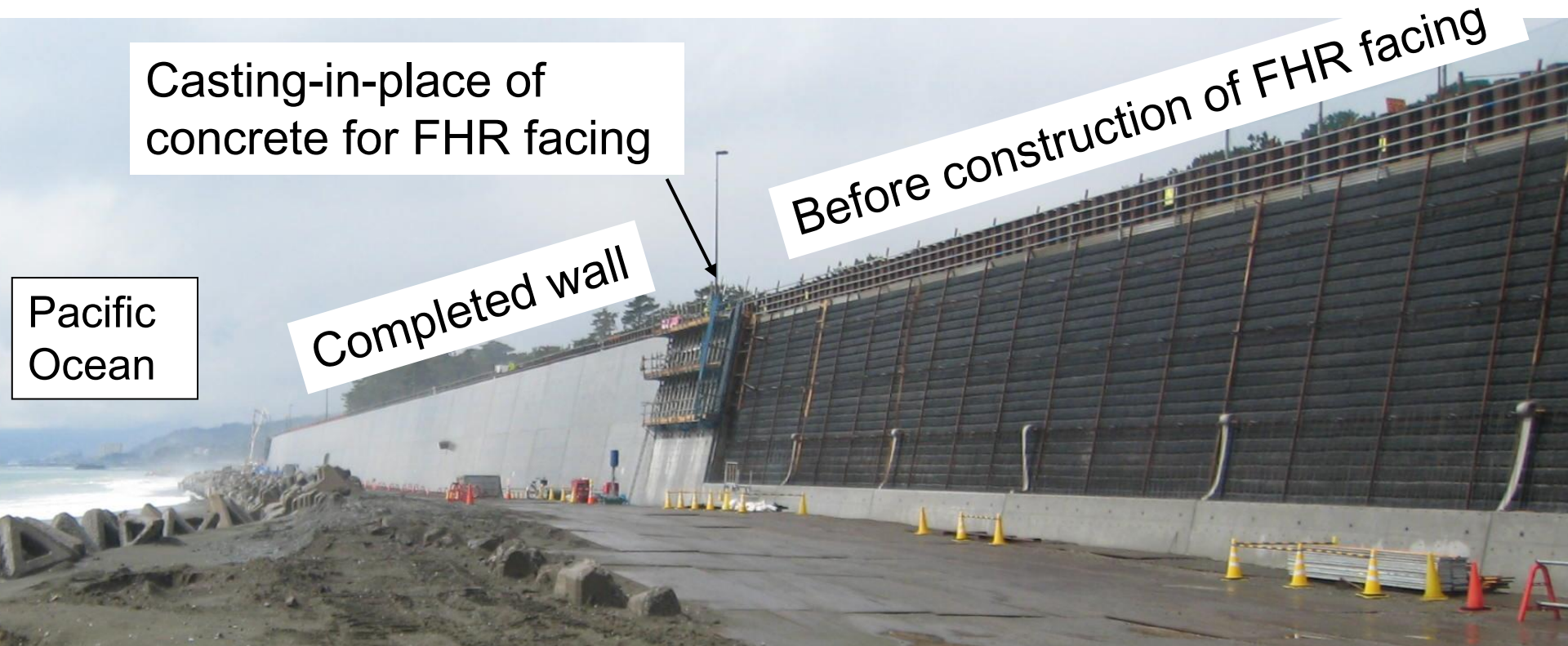
Before collapse:



Restoration:

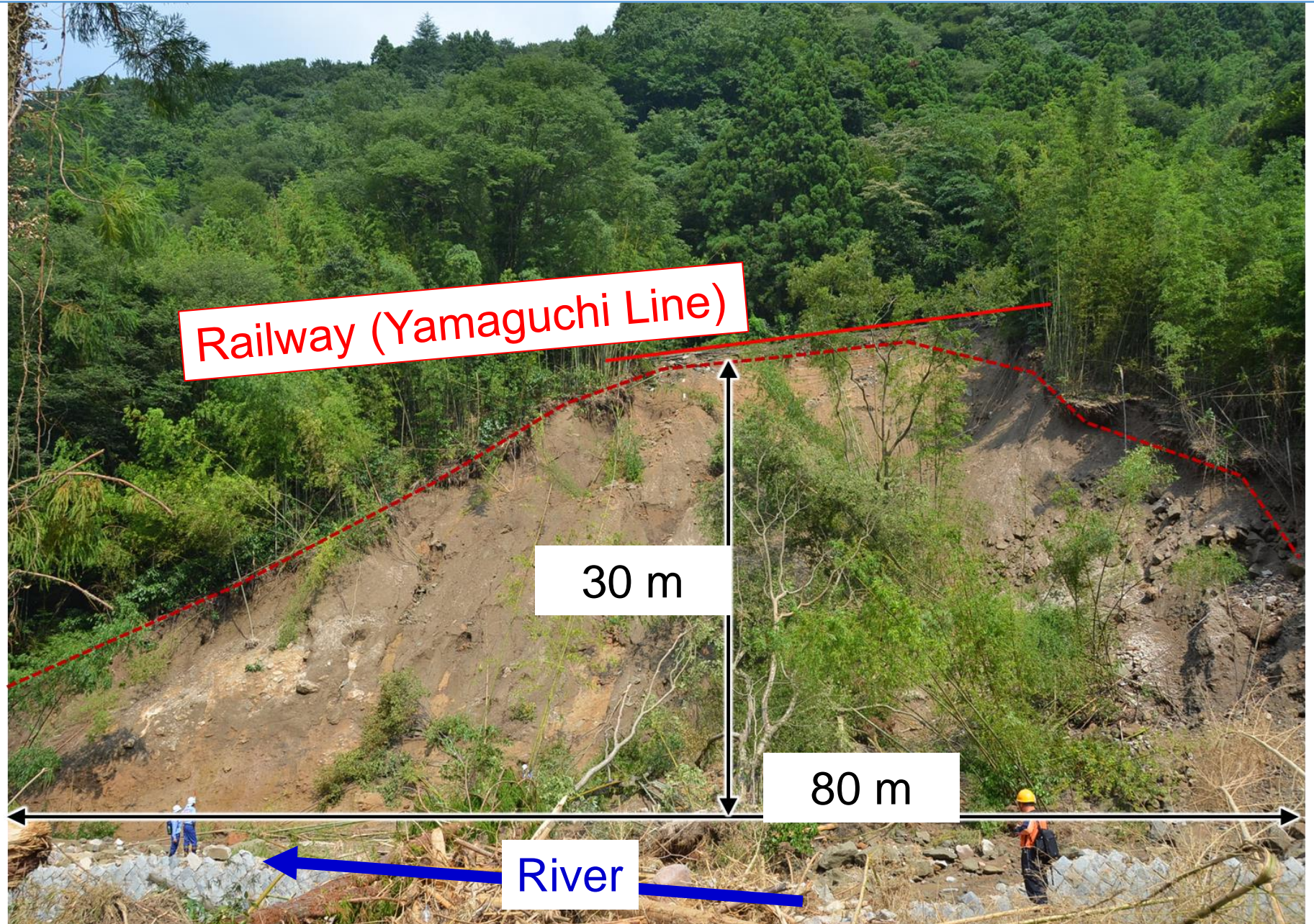


Restoration to GRS RW with FHR facing

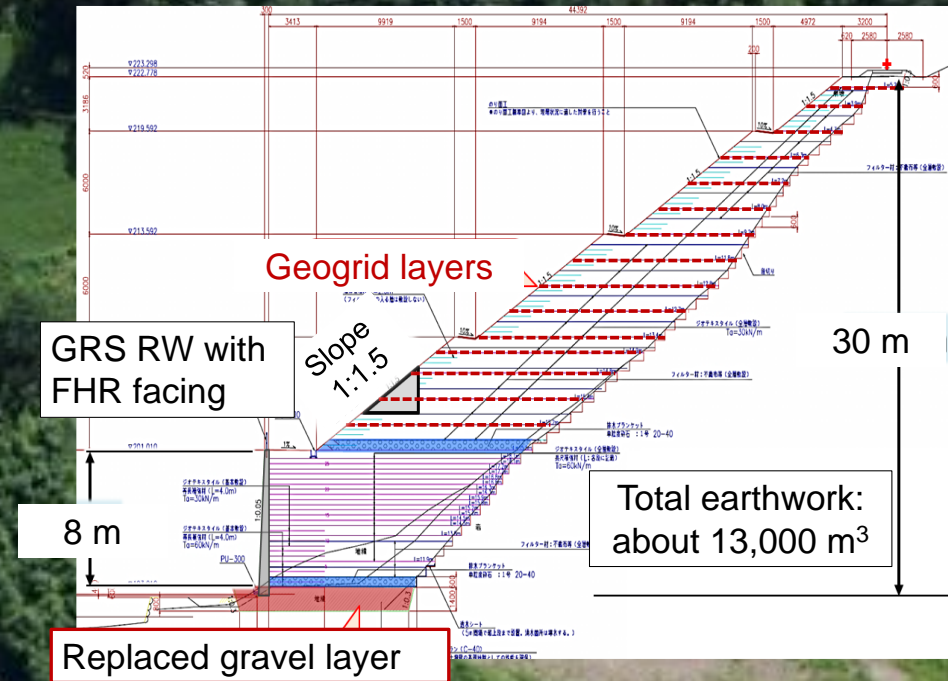
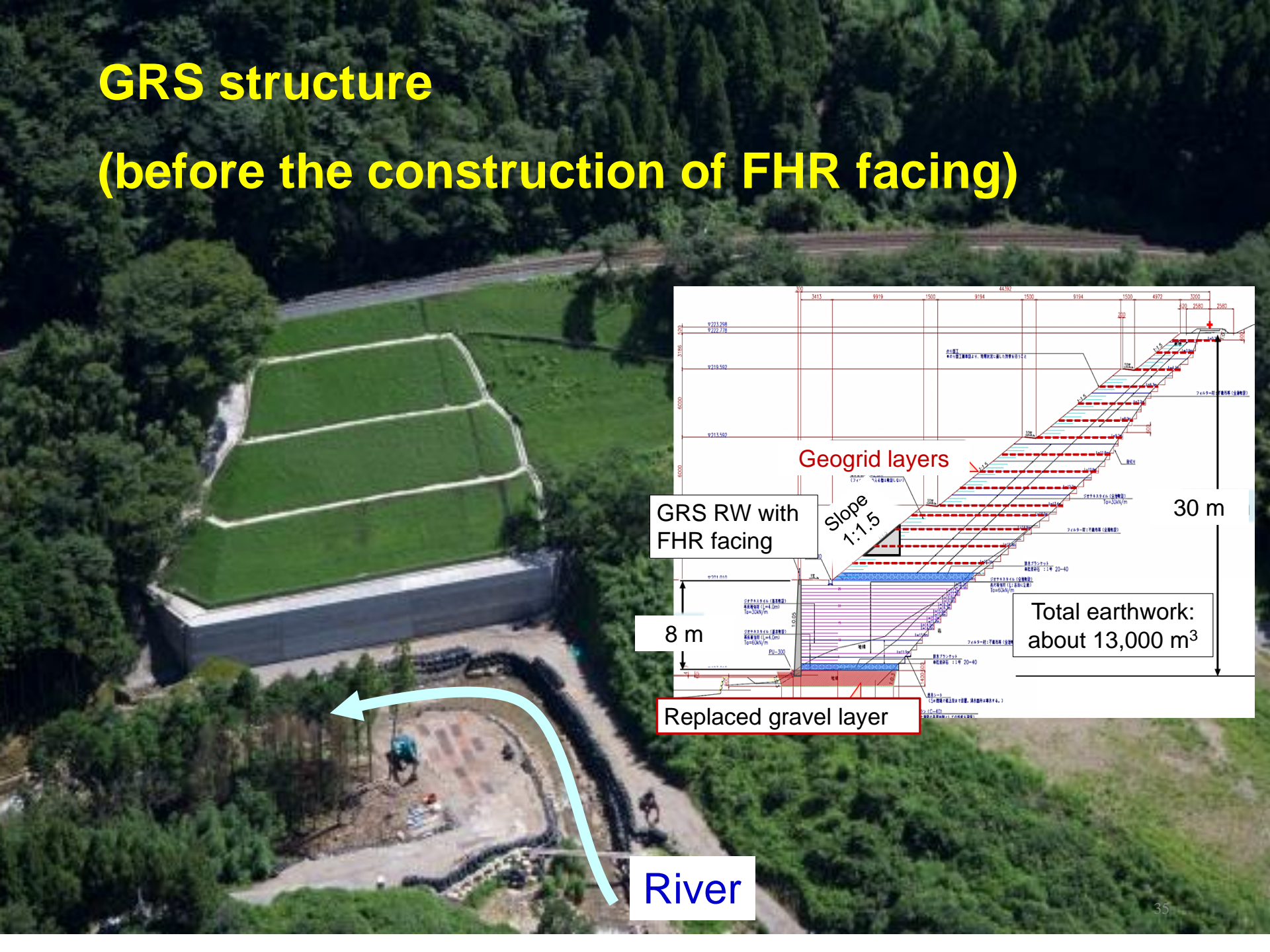


10 March 2010

Collapse of railway embankment by scouring at the toe



GRS structure (before the construction of FHR facing)



River

Completed GRS structure

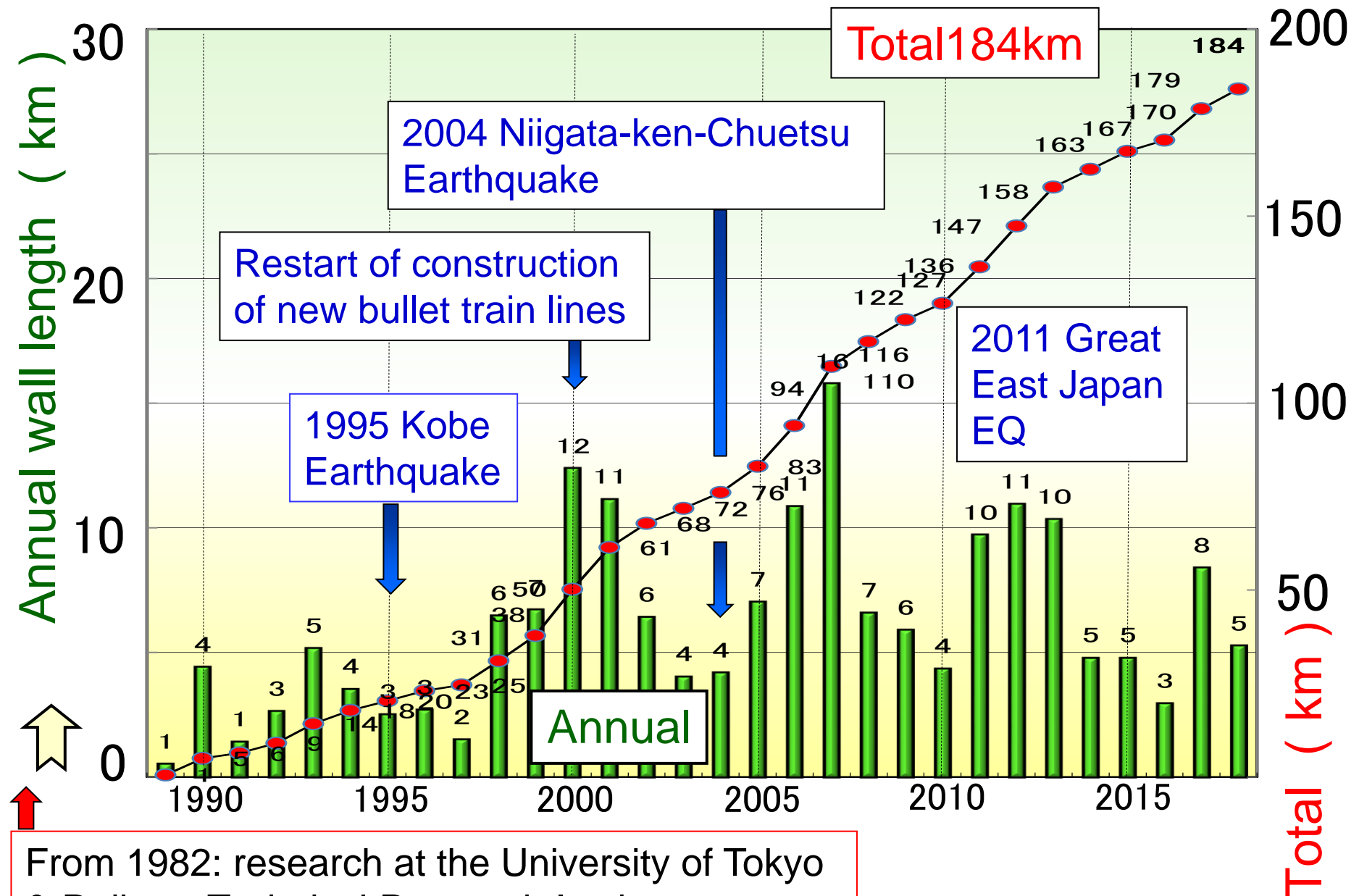
FHR facing to effectively resist scouring

River

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Concluding remarks – 1: Brief history

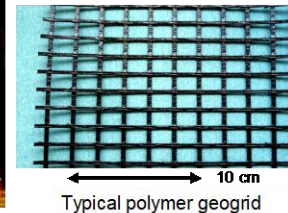
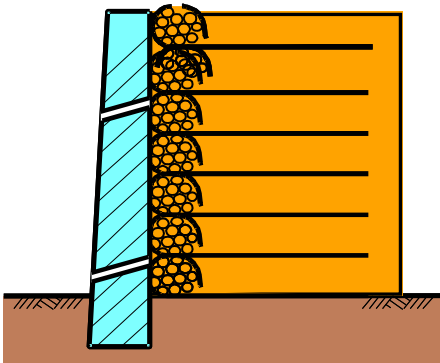


Concluding remarks – 2

GRS RWs with stage-constructed FHR facing and related GRS structures have been constructed as important permanent RWs and other soil structures for a total length of about 190 km, many for railways including high-speed railways (Shinkansen).

Its popular use is due to high cost-effectiveness by:

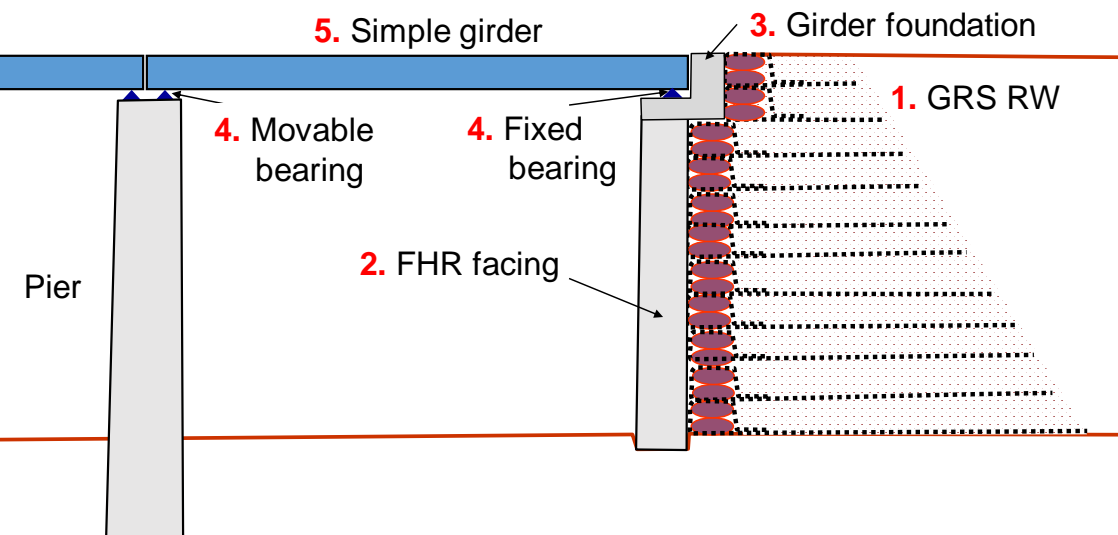
- **high performance** during long-term service and against severe earthquakes, heavy rainfalls etc. and
- **low cost** for construction and maintenance.



Concluding remarks – 3

GRS Bridge Abutment supports one end of a simple girder with a fixed bearing on the top of FHR facing of GRS RW. This is much more cost-effective and much more stable than the conventional type abutment. Since opened to service, all exhibited practically zero bump.

GRS Bridge Abutment is now one of the standard bridge abutments for railways in Japan.



Concluding remarks – 4

GRS Integral Bridge structurally integrates both ends of a continuous girder to the top of the FHR facings of a pair of GRS RWs, not using bearing. This is much more cost-effective and much more stable than the conventional simple girder bridge.

GRS Integral Bridge is now one of the standard bridge systems for railways in Japan.



Concluding remarks – 5

A great number of conventional type embankments, RWs and bridges collapsed during severe earthquakes, heavy rainfalls, floods, tsunami etc. Many of them were restored to GRS structures with staged constructed FHR facing.



Concluding remarks – 6

The following **three breakthroughs** were necessary to develop the GRS technologies explained in this presentation:

- 1) Full-height rigid (FHR) facing** for changes from low earth pressure to high earth pressure in the wall; and from the facing as a secondary non-structural component to a primary structural component for GRS structures.
- 2) Staged construction** for a change in construction from the backfill last to the backfill first.
- 3) Structural integration of the girder to the FHR facings** for a change from statically determinate but unstable conventional soil structures to statically indeterminate but stable GRS structures, in particular GRS Integral Bridges.